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- technology for a sustainable economic development and renewable energy,
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Revista are un *Colegiu de redacție* format din academicieni, profesori universitari și cercetători științifici din România și din străinătate – personalități recunoscute din domeniul științelor ingineresti (în special, din electrotehnică, electronică, automatică și din celelalte domenii ale ingineriei).

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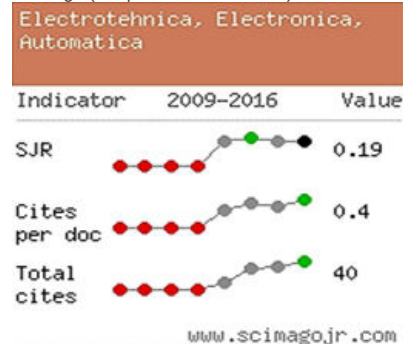
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About

The **Electrotehnică, Electronică, Automatică (EEA)** [Electrical Engineering, Electronics, Automation] is a peer-reviewed scientific journal in the field of the engineering published by "Electra" Publishing House (as part of Icpe).

Scope

The EEA Journal aims to publish only those papers that by the new ideas and the results shown to bring significant contributions to research in the Romanian and international avant-garde engineering as electrical engineering, electronics, automation and other engineering sciences.

Abstracting and indexing

The EEA journal is included in the B+ category by the National Council of Scientific Research in Higher Education (CNCSIS) and indexed in international databases:

Ulrichsweb.com™ (1997-present) (Since 2007, Ulrich's becomes a part of Serials Solutions in the ProQuest family.)

Index Copernicus International (2009)

Elsevier- Engineering Village-Scopus (2012)

Elsevier- Engineering Village-Compendex (2012)

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Currently, EEA is under evaluation by Thomson Reuters - ISI.

Description

The EEA Journal is founded in **1950** under the name „Electricitatea” (ISSN 1220-2533; vol. 1-3) that, in 1953, changed its name in „Electrotehnica” (ISSN 0013-5321; vol. 1-22) that, in 1975, after including „Automatica și Electronica (ISSN 1220-2584), is published under the present name „Electrotehnica, Electronica, Automatica (EEA)” (for further details, please read “History” and “Journal Genealogy” on this site).

Since the early issues, although it was the only scientific journal specialized in the field of electrical engineering, and the EEA has been highly rated thanks to the scientific level of its papers.

The Editorial Board includes academicians, university professors and researchers from Romania and abroad that are well-known personalities in the field of engineering sciences (especially, in electrical, electronics, automation, computer science and other fields of engineering, etc.).

At present, the EEA is recognized as a leader among the scientific publications for the quality and high standards of the papers belonging to the field of engineering sciences. The authors are specialists, researchers and academics from Algeria, Belgium, PR of China, Finland, France, Germany, Italy, Moldova, Slovakia, Hungary, etc.

In the EEA, there are published original papers, that haven't been previously published and are not under consideration for publication somewhere else, as well as papers presented at conferences only if they have not been published (partially or fully) in the proceedings of that scientific event (min. 6 pages, max. 16 pages), syntheses of research projects, scientific debates and syntheses on priority themes of fundamental and applied research (max. 20 pages), reviews / reading notes of the latest scientific and technical books (max. 1 page), commented lists of bibliographic resources in engineering sciences (max. 8 pages).

Papers should be written in English.

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Subcategories »

- History
- Journal Genealogy

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"TECHNOLOGIES FOR A SUSTAINABLE DEVELOPMENT"

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ICPE was founded by the Government Decision no. 868 of 5 August 1950 (under the name „Institutul de cercetări electrotehnice” [Institute of Electrical Research]).

ICPE is a complex structure that covers a wide range of innovative activities connected via the electric profile:

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 - Consulting services* (pre-feasibility studies, feasibility and project studies, evaluation of project proposals, technical projects and implementation, energy management, technical control);

"ELECTRA" Publishing House (founded in 1993) is listed among the publishers recognized by CNCS [National Council of R&D and High Education], starting 2001. So far, 300 technical and beyond books have been published. It is the editor of the journal *EEA*

The *Technological Information Centre* helps in the innovation implementation in economy and society by the dissemination information of the R&D results, technological documentation and operators training in order to facilitate the capitalization results.

ICPE is a brand on the Romanian market and abroad.

By its *HR structure* - as PhD researchers, scientists, doctoral students, master students and associated professors - ICPE has the scientific expertise to approach research topics of national or European level:

- electric vehicle,
- electric propulsion systems for boats,
- smart house, technologies for environmental protection,
- monitoring of environmental factors in the biological reservation (the Danube Delta Biosphere Reservation),
- technology for a sustainable economic development and renewable energy,
- new ecological and biodegradable materials,
- medical equipment,
- IT applications, etc.

Scopul revistei

Revista EEA își propune să publice numai acele articole care atât prin ideile noi, cât și prin rezultatele prezentate, să aducă contribuții importante la cercetarea românească de avangardă din electrotehnică, electronică, automatică, informatică și din celelalte domenii ale științelor inginerești.

Articolele, publicate în două versiuni pe suport de hârtie și online, sunt identice. Accesul liber online asigură o mare vizibilitate articolelor.

Prezentare

Revista EEA a fost fondată în anul 1950 sub numele de „Electricitatea” (ISSN 1220-2533; vol. 1-3) care, în 1953, și-a schimbat numele în „Electrotehnica” (ISSN 0013-5321; vol. 1-22), care, în 1975, după integrarea „Automatica și Electronica (ISSN 1220-2584) apare cu numele actual **Electrotehnică, Electronică, Automatică (EEA)** [ISSN 1582-5175; e-ISSN 2392-828X] (pentru detalii, a se naviga pe site-ul www.eea-journal.ro).

Încă de la primele numere, deși era unica revistă specializată din domeniul electrotehnicii, EEA a fost constant apreciată pentru nivelul științific ridicat al articolelor publicate.

În prezent, EEA este recunoscută ca lider printre publicațiile științifice, pentru calitatea și standardele înalte ale articolelor apărute în domeniul științelor inginerești. Printre autori se numără specialiști, cercetători și cadre didactice din Algeria, Belgia, R.P. China, Finlanda, Franța, Germania, Italia, Moldova, Serbia, Slovacia, Spania, Ungaria etc.

În paginile revistei, se regăsesc lucrări științifice originale care nu au mai fost publicate și care nu sunt luate în considerare pentru publicare în altă parte, cât și articolele prezentate la conferințe, cu condiția să nu fi fost publicate (parțial sau integral) în volumele manifestărilor științifice (min. 6 pagini-max. 16 pagini), sinteze ale unor proiecte de cercetare, dezbateri științifice și sinteze pe teme prioritare din cercetarea fundamentală și aplicativă (max. 20 pagini), recenzii / note de lectură ale celor mai recente apariții de cărți tehnico-științifice (max. 1 pagină), liste de resurse bibliografice comentate din domeniul științelor inginerești (max. 8 pagini).

Pentru a dovedi deschiderea către noile domenii de frontieră, Colegiul editorial a creat o secțiune-varia (*Miscellanea Section*), în care sunt publicate articole a căror tematică aparține altor domenii (matematică, științe socio-umane, științe economice, științele vieții și ale pământului (inclusiv mediul), științe agricole, științe medicale etc.) și care, *tangential*, pot fi corelate cu domeniul științelor inginerești datorită viziunii, conexiunilor și al abordării inedite a subiectelor.

Revista are un *Colegiu de redacție* format din academicieni, profesori universitari și cercetători științifici din România și din străinătate – personalități recunoscute din domeniul științelor inginerești (în special, din electrotehnică, electronică, automatică și din celelalte domenii ale ingineriei).

Revista EEA este clasificată **B+** de Consiliul Național al Cercetării Științifice din Învățământul Superior (CNCSIS) și este indexată în bazele internaționale de date: Elsevier, Scopus, Compendex, ProQuest, EBSCO, Ulrich's, Index Copernicus International. În prezent, este în proces de evaluare de Thomson Reuters - ISI.

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The EEA Journal aims to publish only those papers that by the new ideas and the results shown to bring significant contributions to research in the Romanian avant-garde engineering as electrical engineering, electronics, automation and other engineering sciences.

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To prove the openness to new frontier areas, the Editorial Board has created a *varia* section (*Miscellanea Section*) for papers belonging to other thematic areas (mathematics, social studies, economics, life and earth sciences (including the environment), agricultural sciences, medical sciences, etc.) and, *tangentially*, they are related to engineering sciences thanks to vision, connections and novel approach of the topics.

The *Editorial Board* includes academicians, university professors and researchers from Romania and abroad that are well-known personalities in the field of engineering sciences (especially, in electrical, electronics, automation, computer science and other fields of engineering).

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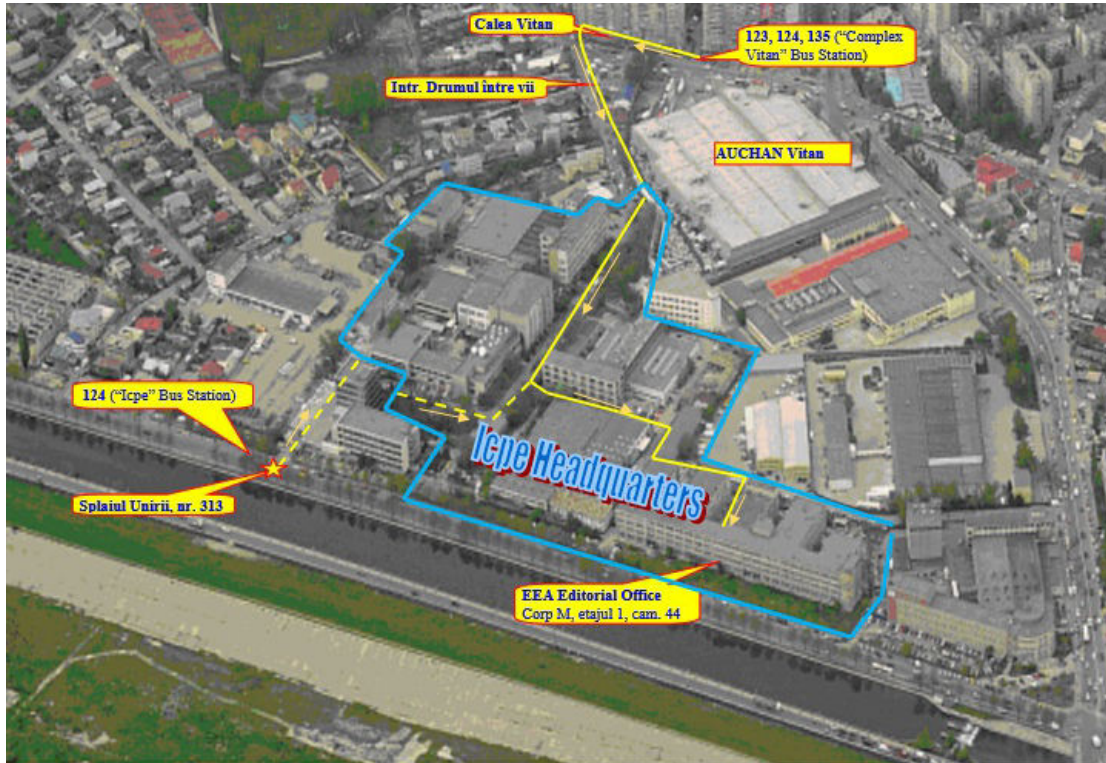
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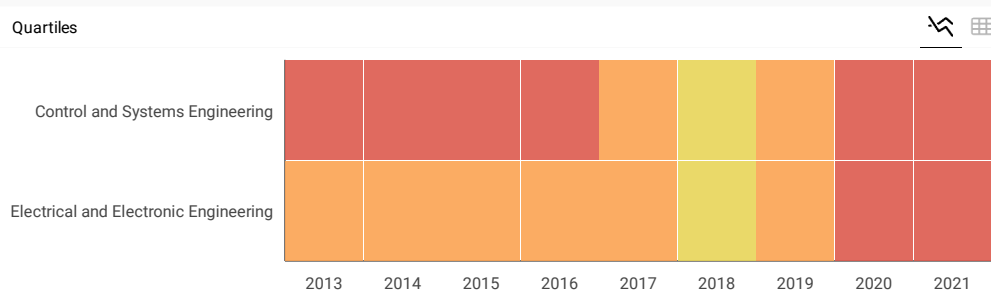
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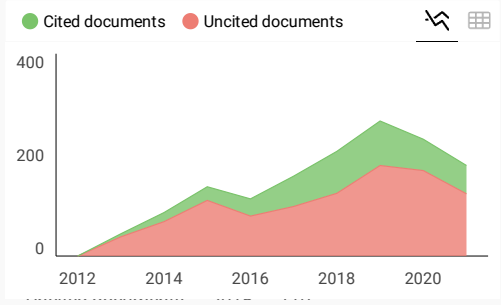
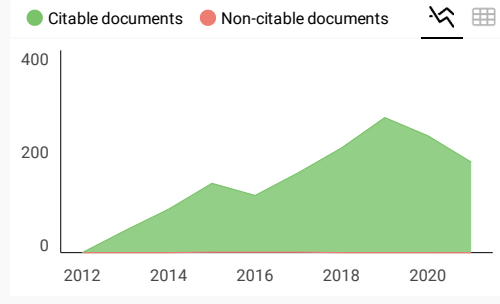
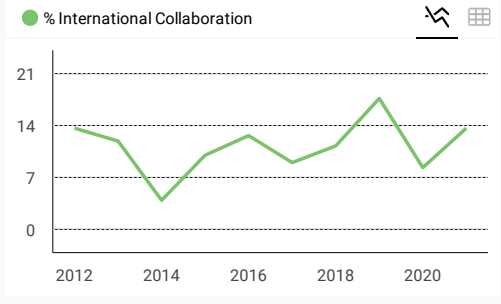
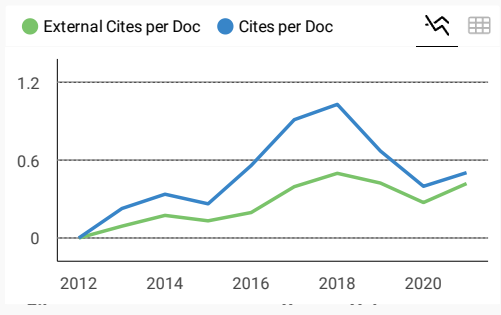
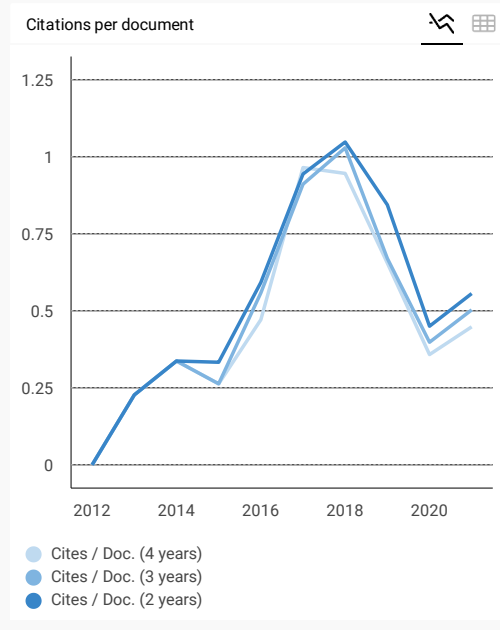
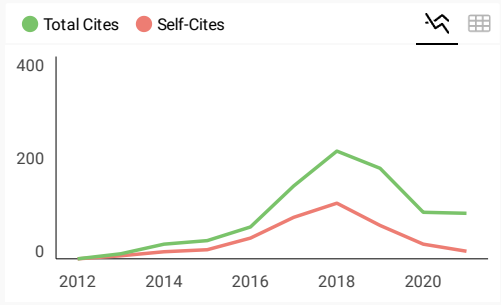
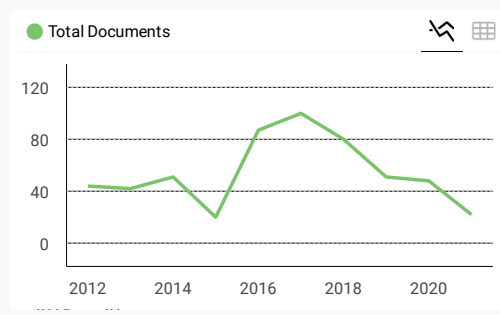
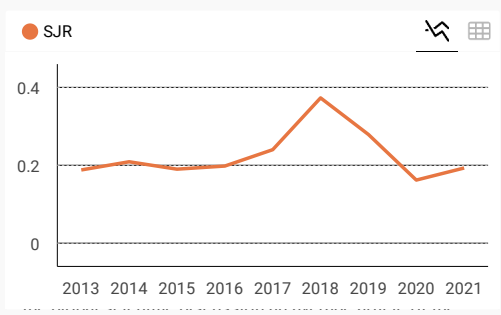
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**Investigation of Transformer Losses and
Temperature Rise**

Waluyo, Siti Saodah, Rohana

Abstract

Power and distribution transformers are very important equipment in a power system. In an application, they experience heating, due to loading. The heating temperature rise has correlations to the loading current, power losses, efficiency and surface area. This research investigated some relations among the power losses, temperature rises, efficiency and the leading current, based on the measurements and empirical approach. The results indicated that the total power and the core losses would increase as the temperature rise increased too, with the average of 0.25 kW/oC and 0.30 kW/oC respectively. The output power increased as the temperature rise rose, as 6.4 kW/oC. Nevertheless, the efficiency would reduce as the temperature rise increased as the average of -6.41 %/oC. The temperature rise was dominantly caused by the power losses, rather than the loading power. By all means, the power losses were significantly depending on the loading power.

Keywords: efficiency, empirical, loading, power loss, transformer, temperature rise

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Investigation of Transformer Losses and Temperature Rise

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Abstract

Power and distribution transformers are very important equipment in a power system. In an application, they experience heating, due to loading. The heating temperature rise has correlations to the loading current, power losses, efficiency and surface area. This research investigated some relations among the power losses, temperature rises, efficiency and the leading current, based on the measurements and empirical approach. The results indicated that the total power and the core losses would increase as the temperature rise increased too, with the average of 0.25 kW/°C and 0.30 kW/°C respectively. The output power increased as the temperature rise rose, as 6.4 kW/°C. Nevertheless, the efficiency would reduce as the temperature rise increased as the average of -6.41 %/°C. The temperature rise was dominantly caused by the power losses, rather than the loading power. By all means, the power losses were significantly depending on the loading power.

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1. Introduction

Power and distribution transformers represent the largest portion of capital investment in transmission and distribution substations. Its importance is an obvious axiom in modern power systems. Transformer outages have a considerable economic impact on the power system operations. Transformers are major components in power systems [1-6]. Overloading of transformers can become necessary in open electricity markets due to economic reasons or simply to ensure continuous energy supply. During an overload circle accelerated ageing and damages have to be strictly avoided [7-8]. It was assessed the state of transformer research in some countries [9-10]. It is essential to carefully study its thermal behaviour [11-12]. One of the most important parameters governing a transformer's life expectancy is the hot-spot temperature (HST) value. The classical approach has been established to consider the hot-spot temperature as the sum of ambient temperature, top-oil temperature rise and hotspot-to-top-oil temperature gradient [13-16]. For transformer cooling when load changes, transformer oil is better than silicon oil [17-18]. The calculations were needed to design a transformer. The optimization algorithms improved the model adequacy, consistency as well as accuracy [19-20]. The toolbox using GUI has been developed for the transformer tests [21]. The model parameters and the precise calculation of power losses distribution were needed. The distribution and power transformers can be in the challenging future smart grid. [22-23]. The simulation of transitional airflow onto a flat plate of transformer was validated through the experiments. The no-load losses consisted by the hysteresis and eddy current losses [24-25]. The load loss of a transformer consists of losses due to ohmic resistance of windings and additional losses, such as

stray losses. The temperature rise was caused by both Joules and stray losses. The ageing of transformers is influenced by short term and long term over loads, number and intensity of short circuits, incidence of lightning, and internal faults [26-29]. The consumers have become increasingly aware of fires and explosions involving oil-filled transformers located in power plants or substations. The winding loss was to add the obtained asymmetric magnetization current to the load currents [30-31].

There are two kinds of transformer thermal models, IEEE TOT/HST and ASU TOT/HST models [32]. The temperature rise test is to evaluate the methodology being currently used in the industry and to propose improvements by applying concise analysis, electrical power engineering principles and optimization theories in order to increase measurement accuracy while also reducing test performance times. The affecting factors of winding temperature rise are winding resistance, ambient temperature, oil temperature, load loss and core temperature [33-34]. The thermal effect, moisture, acidity, oxygen, etc were the controlling factor in determine transformer lifetime. For every 1 °C ambient temperature reduction, from standard 30 °C, releases approximately 1 % of overloading capability [35-36]. Thermal aspects affect transformer design. Therefore, the heat transfer at the winding surface is determined by the cooling conditions. Transformers ageing are one of the critical issues utilities [37-38]. The increased transformer loss caused by non-linear loads leads to an increase in transformer temperature, fatigue and premature failure. The losses in the windings and the core cause temperature rises in the materials. The most warm up parts of transformer were coils, and then core and oil [39-41]. The ONAN type transformers may lead to more general and more reliable recommendations regarding the influence of different heat sources space distribution.

The intensity of thermal ageing is dependent on the hot-spot temperature [42-43].

The limitation on the loss of life of the insulation and the winding hottest-spot temperature are the driving factors for overload limits. It gives a better understanding of the thermal performance of the transformer and it can be built up before the transformer is manufactured. The hot-spot temperature is not strongly influenced by the value of the hot-spot factor. The hotspot temperature of disc windings has a close relation with the transformer age due thermal behaviour. The degradation of electrical insulation in transformers is traced to thermoelectric processes. The hot spot temperature depends on instantaneous load, ambient temperature, winding design and cooling model. The oil temperature rise would be reduced by increasing the number of ribs and enlarging their dimensions. Dimensional changes made to the optimized cooling, increased oil cooling efficiency and significant cost savings. A monitoring system was considered essential to ensure reliability and sustainability of the transformer. Thermal design of oil-cooled transformers is generally done by empirical lumped parameter methods. Consideration of significant variation of ambient temperature into transformer thermal dynamics, seems a questionable from the thermodynamically point of view. Maximum hot-spot temperatures and relative loss of life may be underestimated when transformer operates under larger and severe overloads and with correlation between load and ambient temperature. If a transformer becomes too hot internally, then the insulation materials will degrade faster and the operating lifetime of the transformer will be shortened. Transformers in presence of winding short circuit faults are most important causes of failures. The estimating concept of overloading and thermal performance could be simplified as a thermal model. This is equivalent to limiting the aging acceleration factor (rate of loss of insulation life) to a pre-determined limit. The largest influence came from the top oil temperature where the variable viscosity test cases produced temperatures approximately 20 °C higher than the constant viscosity cases. The higher overload of the error is more pronounced as the oil viscosity effect [44-61].

Air temperature distribution was quite uniform but it possess a heat reservoir for the heated oil within the transformer. The loading guide offers relations for the calculation of the HST based on per-unit load. The insulation hot-spot temperature was the most critical quantity during transformer loading. The temperature was needed to consider when developing transformer-aging models. The top oil temperature and hot spot temperature as two criteria to evaluate the load ability and the insulation life of transformer. The effect of thermal stress was on the lifetime of the transformer [62-68].

The life of a transformer depends on the life of its insulation system and it is primarily dependent on transformer operating temperature.

The hottest-spot temperature and the exposed time reduce the mechanical tensile strength and the degree of polymerization of insulation. The hot-spot temperature values are used to calculate aging parameters, which include the aging acceleration factor, time dependent relative aging rate and insulation life loss. The loads or temperature ranges were wide or arithmetic it presents considerable values. The essential knowledge for a transformer reliable operation was achieved by using thermal transformer models.

The harmonic distortion can cause unnecessary winding loss and typical temperature rise, and decreases its life expectancy. [69-75]

The objective of research was to investigate the transformer losses and temperature rise based on the empirical equation and the sample of temperature measurements. Based on these parameters, it could be calculated the losses, output powers, and efficiency against to the temperature rises and the load currents.

2. Materials and Methods

The technical data of the transformer are 1 MVA, 50 Hz, 28.90 A, Dyn5 of vector group, 6.0 % of impedance, 2.52 tons. For this transformer, the nominal no load and load losses (P_0 and P_k) were 2.3 kW and 9 kW respectively. Finally, by the calculation, the transformer surface area (A_t) was 117,684 cm².

The output power from the transformer was less than the input power. A much power distinction is converted into heat by core and winding losses. A combination of radiation and the heat dissipated is from the unprotected surface of transformer. The dissipated heat depends on the total surface area that is unprotected from the original core transformer and the total surface area that is not protected from the windings. The temperature rise in the transformer is difficult to predict precisely. One approach was to combine losses in the winding with core losses in transformers and assumed the heat energy dissipated uniformly through the surface to the core and winding of transformer at ambient temperature conditions. It is not a bad assumption considering most transformer surface area is the ferrite core winding rather than winding area with thermal conductivity (around 40 mW/cm²/°C) is poor at any temperature. With these assumptions, the amount of temperature rise in a transformer could be calculated by the following formula [76].

$$\Delta T = \left(\frac{P\Sigma}{A_t} \right)^{0.833} \quad (1)$$

where ΔT , $P\Sigma$ and A_t were temperature rise (°C), total transformer losses (mW/cm²) and transformer surface area (cm²).

$$P\Sigma = P_0 + P_k \quad (2)$$

where P_0 and P_k were no load and load losses respectively.

$$P_0 = \frac{V^2}{R_i} \quad (3)$$

$$P_k = kI^2 \quad (4)$$

For three phase power

$$P = \sqrt{3} V I \cos \phi \quad (5)$$

Power efficiency of transformer is

$$\eta = \frac{P_{out}}{P_{in}} \times 100\% \quad (6)$$

3. Calculation Results and Discussion

From the results of calculations, it could be calculated the power losses against the temperature rise which can be seen in Figure 1 below.

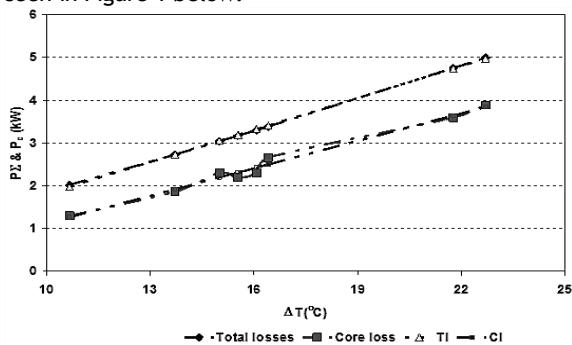


Figure 1. The power losses versus the temperature rise

It is seen that the core and total losses linearly rose as the temperature rise increased. Based on this curve, the total power loss and the core loss output powers would increase as the temperature rise increased too, with the average of 0.25 kW/°C and 0.30 kW/°C respectively. Figure 2 shows the output power as function of temperature rise.

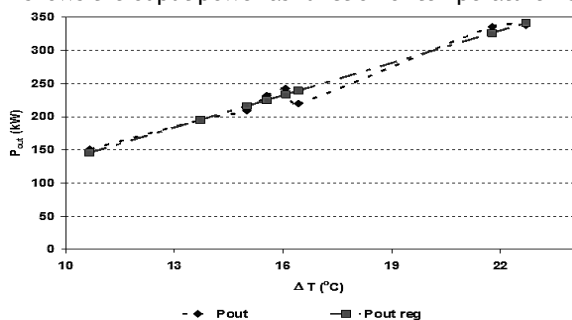


Figure 2. The calculated power output to the temperature rise

Both quantities would rise in proportional. The output power increased as the temperature rise rose, as 6.4 kW/°C. Table 1 lists the data of temperature rises, both measurement and calculation results.

Table 1. Calculation and measurement of temperature rise

Measurement results ΔT (°C)	Calculation results ΔT (°C)
24	10.66
23	15.00
19	21.76
19	22.70
22	13.72
21	15.54
21	16.07
22	16.41

Table 3. Sample of calculation results

S _{rat} (kVA)	Current (A)			Average Current (A)	$P_{k1\phi} = K_{1\phi} \cdot I^2$			$P_{k3\phi R}$ (W)	$P_0 = \frac{V^2}{R_i}$ (W)
	I _R	I _S	I _T		$P_{k1\phi R}$	$P_{k1\phi S}$	$P_{k1\phi T}$		
300	400	417	410	409.0	230.4	250.4	242.1	722.9	1293.9
400	420	410	410	413.3	254.0	242.1	242.1	738.1	2300.2
500	500	550	500	516.7	360.0	435.6	360.0	1155.6	3594.0
520	510	500	510	506.7	374.5	360.0	374.5	1109.1	3887.3
360	410	450	480	446.7	242.1	291.6	331.8	865.4	1863.1
390	450	500	480	476.7	291.6	360.0	331.8	983.4	2186.6
400	430	510	500	480.0	266.3	374.5	360.0	1000.8	2300.2
430	400	400	430	410.0	230.4	230.4	266.3	727.1	2658.1

The difference of the temperature rises between the calculation, and the measurement results were predicted to be caused by the less accurate of reading on the thermometer when the retrieval of data and it took a time for reading the thermometer.

From the calculations those have been done, the efficiencies of transformer depended on the transformer power output, so that when the output power increased, then the temperature rise and the efficiency decreased. Therefore, it was obtained the graph of efficiency against the temperature rise (ΔT), as shown in Figure 3.

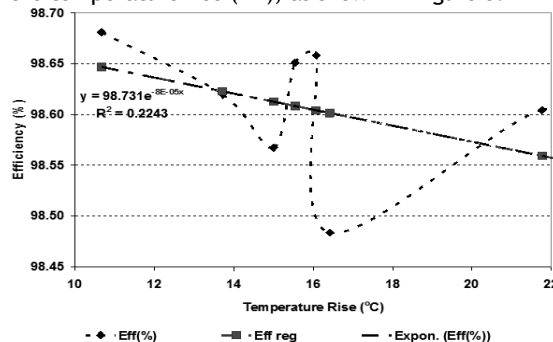


Figure 3. The efficiency to the temperature rise

The increasing temperature rise made the transformer efficiency fairly reduced. The efficiency would reduce as the temperature rise increased as the average of -6.41 %/°C.

Table 2 lists the sample of measurement results.

Table 2. Sample of measurement results

No	Time	Voltage (Volt)	Current (A)			Average Current (A)	Cos φ	ΔT (°C)
			I _R	I _S	I _T			
1	08.00	300	400	417	410	409.0	0.71	24
2	09.00	400	420	410	410	413.3	0.73	23
3	10.00	500	500	550	500	516.7	0.75	19
4	11.00	520	510	500	510	506.7	0.74	19
5	12.00	360	410	450	480	446.7	0.70	22
6	13.00	390	450	500	480	476.7	0.72	21
7	14.00	400	430	510	500	480.0	0.73	21
8	15.00	430	400	400	430	410.0	0.72	22

Nevertheless, the average current values were based on the three phase of currents. It is shown that the voltage, current and power factor changed on every hour measurement. Nevertheless, generally, the temperature rises would increase as the load currents rose.

Table 3 lists the calculation samples of current and powers.

Generally, the powers would increase as the currents efficiency and temperature rise calculation results. rose. Table 4 lists the calculation samples of power,

Table 4. Sample of power, efficiency and temperature rise calculation results

$P_{\Sigma} = P_o + P_k$ (W)	$P_{out \ 1\phi} = \frac{V}{\sqrt{3}} \cdot I \cdot \cos \phi$ (kWatt)			$P_{out \ 3\phi}$ (Watt)	$P_{in} = P_o + P_k + P_{out}$ (Watt)	η (%)	$\Delta T = \left(\frac{P_{\Sigma}}{At} \right)^{0.833}$ (°C)
	P_{out-R}	P_{out-S}	P_{out-T}				
2016.7	49.2	51.3	50.4	150.9	152.9	98.68	10.66
3038.3	70.8	69.1	69.1	209.0	212.1	98.57	15.00
4749.6	108.3	119.1	108.3	335.6	340.3	98.60	21.76
4996.4	113.3	111.1	113.3	337.7	342.7	98.54	22.70
2728.6	59.7	65.5	69.8	195.0	197.7	98.62	13.72
3170.0	73.0	81.1	77.8	231.8	235.0	98.65	15.54
3301.0	72.5	86.0	84.3	242.8	246.1	98.66	16.07
3385.2	71.5	71.5	76.9	219.9	223.2	98.48	16.41

Based on figures 4-7, the output powers would rise quadratically as the loading currents rose.

Figure 4 shows the phase-R power output versus the current magnitude. Generally, the output power would increase quadratically as the loading current rose.

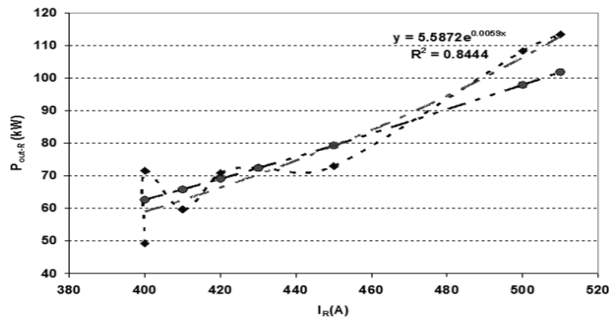


Figure 4. The phase-R power output to the current magnitude

Figure 5 shows the phase-S power output versus the current magnitude. Generally, the output power would increase quadratically as the loading current rose.

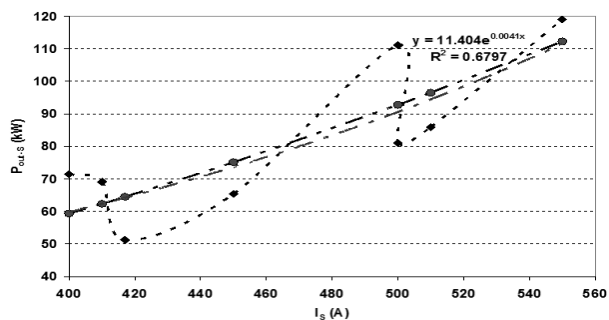


Figure 5. The phase-S power output to the current magnitude

Figure 6 shows the phase-T power output versus the current magnitude. Generally, the output power would increase quadratically as the loading current rose.

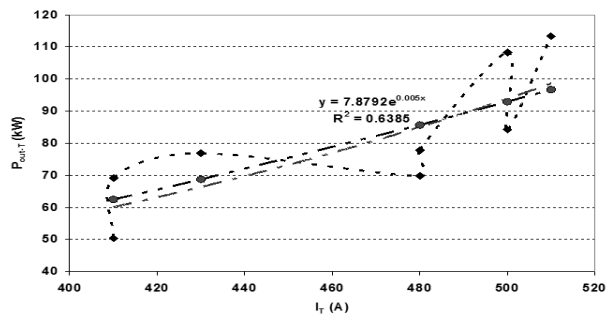


Figure 6. The phase-T power output to the current magnitude

Figure 7 shows the total power output to the average current magnitude.

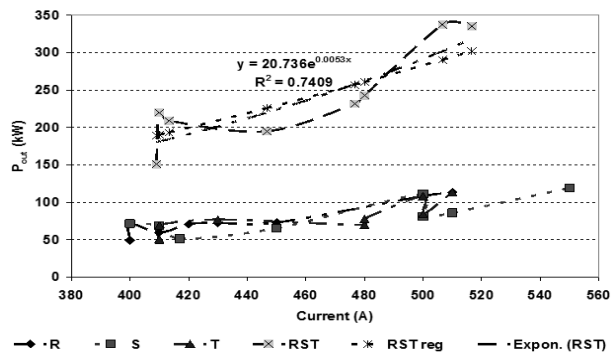


Figure 7. The total power output to the current magnitude

Figure 8 shows the efficiency versus the average current magnitude on three phase.

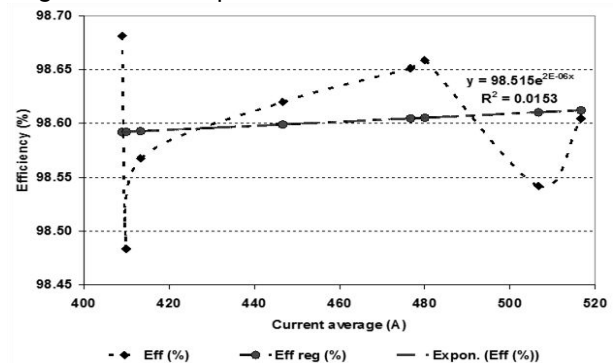


Figure 8. The efficiency to the current magnitude

Figure 9 shows the temperature rise versus the average current magnitude on three phase. The temperature rise would increase quadratically as the current rose.

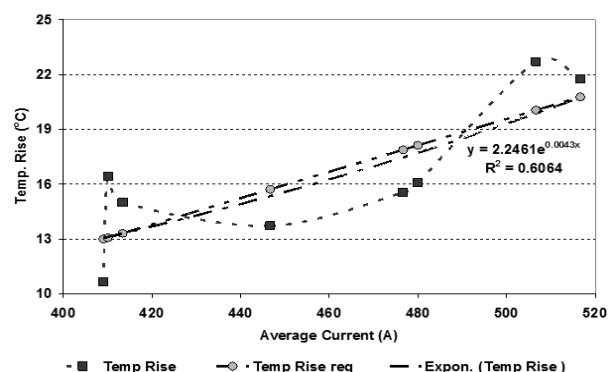


Figure 9. The temperature rise to the current magnitude

Figure 10 shows the core and total losses versus the average current magnitude on three phase.

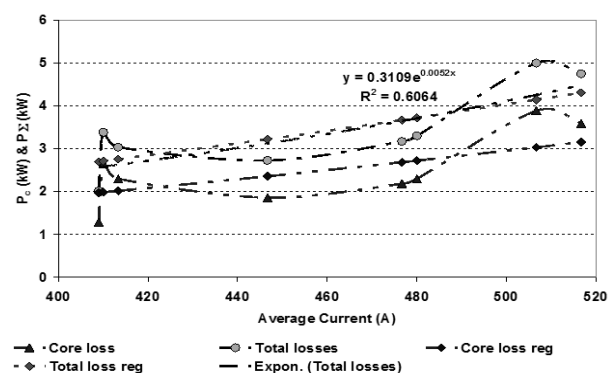


Figure 10. The core and total losses to the current magnitude

Figure 11 shows the correlation between the losses against the output power in linear.

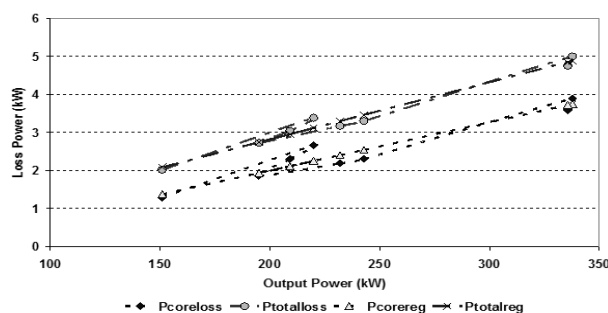


Figure 11. The core and total losses versus the output power

4. Discussion

Figure 1 indicates that the core and total losses were linier to the temperature rise, where the temperature rise increase as the loss as the losses increased too. For this case, the empirical equations are $P_c(kW)=0.214(\Delta T)-1.02$ and $P_\Sigma(kW)=0.249-0.686$ for the core and total losses respectively. If these equations were be reversed, the become $(\Delta T) = 4.67 P_c(kW)+4.766$ and $T=4.016P_\Sigma+2.755$ respectively for core and total losses.

Thus, the temperature rise is strongly depending on the core and total losses, more than four times.

Figure 2 shows the relation chart between the output power and the temperature rise, as the empirical regressive equation is $P_{out}(kW)=16.25(\Delta T)-27.52$ or in reverse $T=0.962P_{out}(kW)+1.694$. Base on this equation, the temperature rise was slightly influenced by the load. Thus, the temperature rise was dominantly influenced by the losses rather than the loading. However, both losses were tightly depending on the output power.

Figure 3 shows that the efficiency would reduce as the temperature rise increased. In the exponential, the relation is $\eta(\%)=98.7e^{-0.00008(\Delta T)}$ or in the linear, the relation is $\eta(\%)=-0.0079(\Delta T)+98.7$. Thus, the temperature rise would determine the efficiency considerably.

Figure 4 shows the correlation of phase-R output power against phase-R loading current, as $P_R(kW)=0.39I^2$ or $P_R(kW)=5.587e^{0.0059I}$.

Figure 5 shows the correlation of phase-S output power against phase-S loading current, as $P_S(kW)=0.37I^2$ or $P_S(kW) = 11.4e^{0.0041I}$. Figure 6 shows the correlation of phase-T output power against phase-T loading current, as $P_T(kW) = 0.37I^2$ or $P_T(kW)=7.88e^{0.005I}$.

While, Figure 7 shows the chart of correlation the total power versus the three-phase average current. The correlation is $P_T(kW)=0.00113I^2$ or $P_T(kW)=20.7e^{0.0053I}$. Based on these correlations, they show quadratically behaviour. However, they are with small constants, tend to be linear.

Figure 8 indicates the correlation of efficiency versus the average current. Based on these data, the efficiency would increase slightly as the average current increased. This correlation is $\eta(\%) = 0.0001875I_{av} + 98.5$ or $\eta(\%)=98.5e^{2E-6I}$.

Figure 9 shows the chart of temperature rise against the average current. The correlation tent to be linear. In the exponential, the correlation is $\Delta T(^{\circ}C)=2.246e^{0.0043I}$ or in linear, it is $\Delta T(^{\circ}C)=0.072I-16.5$.

Figure 10 shows the chart of core and total losses against the average current. The correlation tent to be quadratic. In the quadratic equations, the correlations are $P_o(kW)=0.000012I^2$ and $P_\Sigma(kW)=0.000016I^2$ respectively for the core and total losses.

In figure 11, the regression is $P_{coreloss} = 0.01267P_{out}-0.53$, or reverse it is $P_{out}=78.92P_{core}+41.825$. On the other hand, $P_{totalloss}=0.015P_{out}-0.18$, reverse it is $P_{out}=66.64P_{totalloss}+12$. Thus, the output power tightly depended on the core and total losses.

Based on above figures, the linear graphics were the core and total losses versus the temperature rise, the output power versus the temperature rise and the loss power versus the output power. Therefore, it is said the losses, the output power and the temperature rise were closely correlated. Thus, the temperature rise was dominantly caused by the losses, rather than the loading power. Nevertheless, the power losses were significantly depending on the loading power.

5. Conclusions

From the yielded calculations, the temperature rise were obtained for power ouput on the transformer. The greater the total power losses, the greater the temperature rise. Nevertheless, it was depending on the power output of transformer.

The temperature rise largely increased, the transformer could lead to decline the transformer performance, that by indicated smaller of the transformer efficiency. The temperature rise was dominantly caused by

the power losses, rather than the loading power. Indeed, the power losses were significantly depending on the loading power.

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